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T.L. Johnson page 1 Finite-State Compusators for Continuous Processes

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FINITE-STATE COMPENSATORS FOR CONTINUOUS PROCESSES

T. L. Johnson

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INTRODUCTION

The feedback interconnection of a continuous finite-dimensional dynamic system and a finite state sequential machine is shown in Figure 1. Because the natural input and output spaces of such systems are defined over different fields, two coupling elements, termed a coder and decoder; are necessary to define the transformations of plant output to compensator input, and conversely. There is an extensive literature dealing with each of the foregoing elements, for instance: Willems (1972) defines a dynamical systems theory of continuous processes (the plant); Bobrow and Arbib (1974) review automata theory

(the sequential machine); and Gallager (1968) treats communications theory (the coder and decoder). Considerable progress has been made in the last decade, with the emergence of mathematical systems theory, toward a unifying view of these disciplines—the works of Kalman, Falb and Arbib (1969) and Padulo and Arbib (1970) being representative of a broader literature.

The purpose of the present note is to pinpoint the shortcomings of existing theories when applied to the situation of Fig. 1 and to propose a representation for the state of

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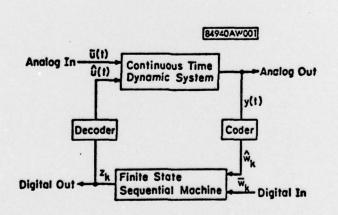
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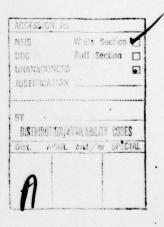


Figure 1: Block Diagram of Finite-State Compensation of a Continuous Process

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such systems. Such a representation provides the cornerstone of a theory for the direct design of finite-state compensators for continuous processes, which subsumes purely continuous control systems and purely finite-state feedback systems as special cases.

THE STATUS QUO: SOME NECESSARY IN-NOVATIONS

In motivating the new representation, it is most appropriate to recount the status quo:

(a) Continuous Dynamic Systems:

These are characterized (Willems and Mitter, 1971) by sets of the form $\Sigma = (U, U, Y, Y, X, \phi, r)$ where

- U: input set
- U: input space
- Y: output set
- Y: output space
- X: state set
- φ: state transition map
- r: read-out map

where U, Y are usually taken as Euclidean vector spaces on the field of real numbers, R, U: $T \rightarrow U$ and Y: $T \rightarrow Y$ are normed linear spaces on the time interval $T \subset R$. The system Σ will be assumed finite-dimensional in this discussion and X is correspondingly taken as a Euclidean vector space. The state transition mapping is continuous, with

- ϕ : T x T x U x X \rightarrow X, and the readout map
- r: T x T x U x X + Y is continuous.

In addition, ϕ is required to have the identity, causality, and semigroup properties:

- (i) φ(t,t, u(·), x) = x for all teT,u(·)εU, xεX.
- (ii) For any $t \ge t_0$, both elements of T, and any $x_0 \in X$ if $u_1(\tau) \equiv u_2(\tau)$, $\tau < t$, then $\phi(t, t_0, u_1(\cdot), x_0) = \phi(t, t_0, u_2(\cdot), x_0)$.
- (iii) For any $t_2 \ge t_1 \ge t_0$, all elements of

the form $M=(W, Z, Q, \delta, \lambda)$ where the finite sets W, Z, and Q are the input, output, and state sets, respectively; and $\delta\colon I\times W\times Q+Q$ $\lambda\colon I\times W\times Q+Z$ are the next-state and current output mappings, respectively. The timeset I is taken as a sub-interval of the integers. (The notation has been slightly modified from that of the literature to conform with part $(a)^1$.) The machine is thought of as the recursion $q_{k+1}=\delta(k,u_k,q_k)$ for any $k\geq k_0 \in I$, and the output map $\lambda(k,u_k,q_k)=z_k$. It should be noted that ϕ of part (a) is analogous to $\delta(k,u_k,\delta(k-1,u_{k-1},\delta(k-2,\ldots,u_{k_0},q_{k_0})\ldots)$, the composition of δ with itself $k-k_0$ times.

(c) Coding and Decoding:

Let A, B denote (finite) alphabets and let A^+ (B^+) denote the set of non-empty finite-length sequences of elements from A(B). Let $h: A^+ \Rightarrow B^+$ be a homomorphism; then the set $h(A) = \{h(a) \mid a \in A\}$ is termed a <u>code</u>. h(A) is uniquely decodable iff h is an injection.

These definitions summarize standard results from the theory of noiseless channel coding; see also Gallager (1968).

The objective of the next section is to characterize the interconnection shown in Fig. 1 as a dynamic system of some general class. Evidently, (a)-(c) are not directly compatible in their present condition. This is partly a problem of notation and technicalities, but there remain some fundamental difficulties. In (c), for instance, one would like the alphabet A to be real rather than finite-valued; but so long as B is finite, h(.) could never be an homomorphism. In (b) and (c), the real-time sequence of state transitions has been abstracted, and only the ordering of transitions remains; but for continuous dynamical systems as in (a), actual transition times in t(t) must be preserved. The basic operations on the fields in (a) and (b) are different, and thus the class of possible functions generated by & and A are inherently different. Finally, it might be necessary to generalize the input space of (a) to include distributions (i.e., impulse trains).

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- (iii) For any $t_2 \ge t_1 \ge t_0$, all elements of T, any $u(\cdot) \in U$, and any $x_0 \in X$, $\phi(t_2, t_0, u(\cdot), x_0) = \phi(t_2, t_1, u(\cdot), \phi(t_1, t_0, u(\cdot), x_0))$.

The system is thought of as the pair of equations $x(t) = \phi(t,t_0, u(\cdot), x(t_0))$ and $y(t) = r(t, t_0, u(t), x(t)), t \ge t_0$ both in T. Referring to Fig. 1, the input u(t) may be taken as the pair $(u(t), \hat{u}(t))$.

(b) Finite-State Sequential Machines (Finite Automata):

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PROPOSED REPRESENTATION

By introducing some formal assertions, we demonstrate how definitions (b) and (c) may be modified so that the system of Fig. 1 may be interpreted as a generalized dynamical system. The demonstration that these assertions are

By allowing δ, λ to depend on kEI, the structure of the next-state and current-output mappings may vary with k. While W could denote any input string of finite length, it is proper here to associate it with an input set as used in [a]. The initial state q_k and index k_0 are pot specified in the definition of M.

consistent is beyond the scope of this brief note. First, a definition is introduced that generalizes the machine M to have a : real-time structure.

Definition 1: A finite-state dynamic system, on an interval TCR, is a set $\Gamma = (\widetilde{W}, \widetilde{W}, \widetilde{Z}, \widetilde{I}, \widetilde{Q}, \widetilde{\delta}, \widetilde{\lambda})$. The sets $\widetilde{W} = TxW$ and $\widetilde{Z} = TxZ$ for finite input and output sets W,Z respectively. and Z are spaces of sequences of elements in W and Z for which the first index is monotonically increasing. For a positive integer n and finite set Q, the state set has the structure $\widetilde{Q} = (TxQ)^n$. The state-transition map $\widetilde{\delta}$: $TxTx\widehat{W}x\widehat{Q}+\widehat{Q}$ satisfies the following properties: Given a sequence $\{\widetilde{w}\} = \{t_k, w_k\} \in \widetilde{W}, \text{ let } T_k \text{ denote the pro-}$ jection of w onto T, i.e., the set of input transition-times $\{t_k\}$, $k=k_0$, k_0+1 , k_0+2 ,.... For any $\{\widetilde{w}\}\in\widetilde{W}$, t_i , t_i , $t_i\in T_k$, $\widetilde{q}\in \widetilde{Q}$, then

- $\delta(t_1,t_1,\{\tilde{w}\},\tilde{q})=\tilde{q}$ (i)
- for any ti < ti and {w} EW such that $\{\widetilde{\mathbf{w}}\}^1 \equiv \{\widetilde{\mathbf{w}}\}$ on $\{\mathbf{t}_i, \mathbf{t}_j\}$, then $\widetilde{\delta}(\mathbf{t}_j, \mathbf{t}_i, \mathbf{t}_j)$ $\{\tilde{w}\}^{1}$, q) = $\delta(t_{1}, t_{1}, \{\tilde{w}\}, q)$.
- (iii) whenever $t_i < t_j < t_\ell$, $\delta(t_\ell, t_i, \{\tilde{w}\}, \tilde{q}) =$ $\delta(t_{q},t_{q},\delta(t_{q},t_{q},\{\widetilde{w}\},\widetilde{q})).$

Finally, the readout map λ : TxTxWxQ + Z.

A more concise definition of a finite-state dynamic system could be given if it were not for our attempt to clarify how the conventional notions of dynamic system and finitestate sequential machine have been reconciled. Actually, the ideas are quite simple. The key concept is that all "spontaneous" state transitions should ultimately be attributable to either the initial state or some input transition; the rate at which such transitions occur is due to any inherent finite delays for any implementation of the machine. Consequently, each "input" can be characterized by

- (a) the time of the current input transition, tk
- (b) the new input value (for t ≥ t_k)

This is denoted as $\tilde{w} = \{t_k, w_k\}$ above. Notice that when there are several input lines, a transition on any one of them is considered a transition time. The state set is also a

elapsed time since the most recent (or n most recent) state transition(s), at the current input transition time, t. Between in-

put transitions, the state may, of course, undergo a large (but finite) number of transitions at intervals determined by the internal system delays. However, these are completely predictable given the past state and the current input, and hence the next state can be computed. This is considered to be the key defining property of the "state" of a system. A major technical obstacle in defining real-time automata has thus been successfully removed -- it would otherwise be impossible to project the "next state" of such a system until the "next" input transition were known! Consider now the natural structure of the state-transition map, o between input-transitions t, and t_{k+1} , i.e., $\delta(t_{k+1}, t_k, \{(t_j, w_j)\}, (\tau_k, q_k)^n)$, which is the analog of the next-state map, δ, in a finite-state sequential machine, M. By causality, the map o can only depend on the single pair (tk+1 wk+1) of the sequence {(t, w;)} for a given k. 8 may always be represented as two functions in this

single-transition case:

 $\tilde{\delta} = (\delta_{\tau}, \delta_{q})$ where $\tau_{k+1}^{\ell} = \delta_{\tau}^{\ell}(t_{k+1}, t_{k}, w_{k+1}, (\tau_{k}, q_{k})^{n})$ $q_{k+1}^{\ell} = \delta_{q}^{\ell}(t_{k+1}, t_{k}, w_{k+1}, (t_{k}, q_{k})^{n})$

 $\ell=1,2,\ldots,n$. The function δ_{ℓ}^{ℓ} projects the ℓ -th state transition time, τ_{k+1}^{κ} prior to the current input transition, while the function of projects the current state due to the current input-transition (t_{k+1}, w_{k+1}) . It is readily verified that this definition applies to both synchronous and asynchronous machines. Finally, one can appeal to the viewpoint taken by Allen and Gallager (1977) in viewing the (initial) state of a machine to include both "internal registers" and "mass storage"-thus the compensation algorithm itself becomes part of the machine's initial state. In other words, selecting the control algorithm corresponds to choosing an initial data set for the machine. The formulation is sufficiently general to allow that the algorithm execution changes the machine structure itself. It is approxnately correct to view the ma

W and Z are spaces or sequences of elements in \widetilde{W} and \widetilde{Z} for which the first index is monotonically increasing. For a positive integer n and finite set \widetilde{Q} , the state set has the structure $\widetilde{Q} = (T_KQ)^n$. The state-transition map \widetilde{G} : $T_KT_K\widetilde{W}_K\widetilde{Q}+\widetilde{Q}$ satisfies the following properties: Given a sequence $\{\widetilde{w}\} = \{t_k, w_k\}_E\widetilde{W}$, let T_k denote the projection of \widetilde{w} onto T, i.e., the set of input transition-times $\{t_k\}$, $k=k_0$, k_0+1 , k_0+2 ,.... For any $\{\widetilde{w}\}_E\widetilde{W}$, t_i , t_i , t_i , t_i , t_i , t_i , \widetilde{q}_i , then

- (i) $\widetilde{\delta}(t_i, t_k, \{\widetilde{w}\}, \widetilde{q}) = \widetilde{q}$
- (ii) for any $t_i < t_j$ and $\{\widetilde{w}\} \in \widetilde{W}$ such that $\{\widetilde{w}\}^1 \equiv \{\widetilde{w}\}$ on $\{t_i, t_j\}$, then $\widetilde{\delta}(t_j, t_i, \{\widetilde{w}\}^1, q) = \widetilde{\delta}(t_i, t_i, \{\widetilde{w}\}, q)$.
- (iii) whenever $t_i < t_j < t_\ell$, $\delta(t_\ell, t_i, \{\tilde{w}\}, \tilde{q}) = \delta(t_\ell, t_j, \delta(t_j, t_i, \{\tilde{w}\}, \tilde{q}))$.

Finally, the readout map $\tilde{\lambda}$: TxTxWxQ + 2.

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- (a) the time of the current input transition, t
- (b) the new input value (for $t \ge t_k$)

This is denoted as $\tilde{w} = \{t_{L}, w_{L}\}$ above. Notice that when there are several input lines, a transition on any one of them is considered a transition time. The state set is also a product space; each "state variable" takes values in the finite set Q. The time-parameter carried with it is the time of the most recent state-transition strictly prior to the current input-transition, and qEQ is associated with the value of the state following that state transition; thus elements of \tilde{Q} take the form $(\tau_{\nu},q)^n$, as it may in general be necessary to keep count of a finite number of prior transitions. Again it is important to note that T, is always by convention the

and the _rent in , and he the next state can be computed. This is considered to be the key defining property of the "state" of a system. A major technical obstacle in defining real-time automata has thus been successfully removed--it would otherwise be impossible to project the "next state" of such a system until the "next" input transition were known! Consider now the natural structure of the state-transition map, & between input-transitions t, and t_{k+1} , i.e., $\delta(t_{k+1}, t_k, \{(t_j, w_j)\}, (t_k, q_k)^n)$, which is the analog of the next-state map, δ, in a finite-state <u>sequential</u> machine, M. By causality, the map δ can only depend on the single pair (tk+1 wk+1) of the sequence {(t, w;)} for a given k. 8 may always be represented as two functions in this single-transition case:

 $\tilde{\delta} = (\tilde{\delta}_{\tau}, \tilde{\delta}_{q})$ $\text{where } \tau_{k+1}^{\ell} = \tilde{\delta}_{\tau}^{\ell}(t_{k+1}, t_{k}, w_{k+1}, (\tau_{k}, q_{k})^{n})$ $q_{k+1}^{\ell} = \tilde{\delta}_{q}^{\ell}(t_{k+1}, t_{k}, w_{k+1}, (\tau_{k}, q_{k})^{n})$

l=1,2,...,n. The function δ_I^2 projects the \checkmark ℓ -th state transition time, τ_{k+1}^{ν} prior to the current input transition, while the function of projects the current state due to the current input-transition (tk+1, wk+1). It is readily verified that this definition applies to both synchronous and asynchronous machines. Finally, one can appeal to the viewpoint taken by Allen and Gallager (1977) in viewing the (initial) state of a machine to include both "internal registers" and "mass storage"-thus the compensation algorithm itself becomes part of the machine's initial state. In other words, selecting the control algorithm corresponds to choosing an initial data set for the machine. The formulation is sufficiently general to allow that the algorithm execution changes the machine structure itself. It is approximately correct to view the map δ as the implementation of a machine's "control struc-

Note that $(\tau_k, q_k)^n$ is shorthand for $(\tau_k^1, q_k^1, \tau_k^2, q_k^2, \dots, \tau_k^n, q_k^n)$. In general, n may also depend on k, but is bounded above.

For Continuous Rocassas

page 4

ture", and $\delta_{\bf q}$ as implementing a "data flow structure", in the terminology of computer science.

Returning to the context of the compensation problem, it remains to define the coder and decoder. The following definitions would appear natural:

Definition 2: A dynamic code is a causal mapping $C: Y \to W$. A dynamic decoder is a causal mapping $D: Z \to U$, where Y, U, W, Z are as in the definitions of a continuous dynamical system and a finite-state dynamical system, respectively. Some of the issues of defining codes of this type have been recently discussed by Ziv and co-workers (1977).

Examples

Example 1: Stabilization of a first-order system. Figure 2 shows an unstable first-order lag, which is to be stabilized (if possible) by a D-type flip-flop. The forward-loop is a dynamical system with time-set $T = [0,\infty)$, characterized by 3

 $\Sigma = \{R, C(T), R, C(T), R, \phi, r\}$

where || f || C(T) = sup |f(t)| takes values in the extended real numbers, and

$$\phi(t,t_0,u(\cdot),x_0) = e^{a(t-t_0)} x_0$$
 (4.1)

$$+\int_{t_0}^{t} e^{a(t-\tau-t_0)} u(\tau)dt$$

and

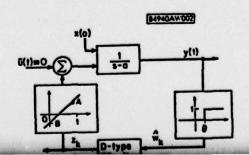
$$r(t,t_0,u(\cdot),x_0) = x(t) = y(t)$$
 (4.2)

The encoder is a threshold function with level θ and binary output, which is sampled at regular intervals $t_k = k\Delta$. The coder input takes values in the space

$$\widetilde{W} = \{\{t_k, \widehat{w}_k\} | k=0,1,2..., \theta_k \in \mathbb{N}, t_k \in \mathbb{R}\}$$

where $W = \{0,1\}$. The coder is then defined by the map $C: C(T) \rightarrow \widetilde{W}$ where for $\{y \in C(T), Cy = \{t_k, \widehat{w}_k\}$ and

Figure 2(a): Stabilization of an Unstable Lag
by a D-Type Flip Flop



R = real numbers; C(T) = cont. functions on

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and - x(t)

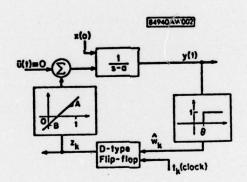
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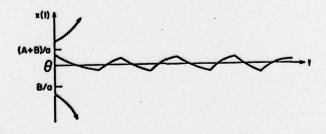


Figure 2(b): Sketch of Typical Responses for Case 2(ii)

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 $\hat{w}_{k} = \begin{cases} 1 & y(t_{k}) \geq \theta \\ 0 & y(t_{k}) < \theta \end{cases}$

The flip-flop is almost the simplest example of a finite-state dynamical system; it is characterized by

 $I_{\Gamma} : \{\widetilde{w}, \widetilde{w}, \widetilde{z}, \widetilde{z}, \widetilde{\varrho}, \widetilde{\delta}, \widetilde{\lambda}\}$

where $\widetilde{W} = Rx\{0,1\}, \ \widetilde{Z} = Rx\{0,1\}, \ and for Z = \{0,1\},$

The state-set is $\widetilde{Q} = (\tau_k, q_k)$ where $\tau_k \in \mathbb{R}$, $q_k \circ Q = \{0,1\}$. In this device, the state merely stores the value of the past input, which was always sampled Δ seconds previously, i.e. $(\tau_k, q_k) = (\Delta, \widehat{w}_{k-1})$. Thus the state-transition map is implemented by

$$\widetilde{\delta}(t_{i},t_{j},\{t_{k},\hat{w}_{k}\},(\Delta,q_{j})) = \begin{cases} (\Delta,w_{i-1}) & i-j \ge 1 \\ (\Delta,q_{j}) & i-j=0 \end{cases}$$

and the output map is

where $\{t_k, z_k\} + f(t)$ is defined by $f(t) = Az_k + B$ whenever $tE[t_k, t_k + A)$ and A, B are real numbers. The design parameters in this feedback system are thus θ , A and B.

The problem of determining which values of x_0 and a>0 yield a Lagrange stabilized system by appropriate choice of θ , A and B has been solved by D. G. Wimpey (1977). Since the system is synchronous, the state-transition maps ϕ , δ may be replaced by one-step recursions, yielding the augmented system⁴

 $\begin{bmatrix} x(t_{i+1}) \end{bmatrix} \begin{bmatrix} e^{a\Delta} & (A/a) & (1-e^{a\Delta}) \end{bmatrix} \begin{bmatrix} x(t_i) \end{bmatrix}$

(ii) If $\theta < 0$, the system is only stable if $x_0 = A/a$, and then x(t) = A/a.

(iii) If $\theta>A/a$, the system is not stabilizable for any x_0 .

(iv) If $0<\theta<A/a$ is chosen properly, a limit cycle is obtained if $0<x_0<A/a$; $x_0=0$ and A/a are critically stable initial conditions.

Case 2: B=0

(i) If B>O, the results are similar to Case 1.

(ii) If B<0, B must be chosen so that (A+B)>0, and θε[B/a, (A+B)/a] leads to a limit cycle about θ. If (A+B)<0, results similar to Case 1 are obtained Initial states x₀ε[B/a, (A+B)/a] may be stabilized.

Most interesting is Case 2, (ii), and a representative trajectory is sketched in Fig. 2(b). The quantity - a\(\) affects the amplitude of limit cycle oscillations.

The purpose of this example is to illustrate how the general notation applies in a specific synchronous finite-state compensation problem, and to illustrate that indeed stabilization of continuous systems may be achieved with a very economical finite-state compensator which can be synthesized with a threshold device, flip-flop, 2-level supply and gate. The proposed representation was used to conceptualize the problem in this case, but is not in itself a design method. Note that the product space for representing the closed-loop system is immediate, given I and I.

Example 2: A Finite-State Dynamical System with Feedback. A simple asynchronous finite-state system, Johnson and Kovacs (1977), with delays in an internal feedback loop is shown in Fig. 3. No general but explicit theory for this class of system is known to the author, yet it is readily represented as a finite-state dynamical system using the proposed framework. Due to space limita-

characterised by

$$/\Gamma : (\widetilde{W}, \widetilde{W}, \widetilde{Z}, \widetilde{Z}, \widetilde{Q}, \widetilde{\delta}, \widetilde{\lambda})$$

where $\widetilde{W} = Rx\{0,1\}, \ \widetilde{Z} = Rx\{0,1\}, \ and for Z = \{0,1\},$

The state-set is $\widetilde{Q} = (\tau_k, q_k)$ where $\tau_k \in \mathbb{R}$, $q_k \in Q = \{0,1\}$. In this device, the state merely stores the value of the past input, which was always sampled Δ seconds previously, i.e. $(\tau_k, q_k) = (\Delta, w_{k-1})$. Thus the state-transition map is implemented by

$$\widetilde{\delta}(\mathsf{t}_{\mathbf{i}},\mathsf{t}_{\mathbf{j}},\{\mathsf{t}_{\mathbf{k}},\widehat{w}_{\mathbf{k}}\},\ (\Delta,\mathsf{q}_{\mathbf{j}})) = \begin{cases} (\Delta,\mathsf{w}_{\mathbf{i}-1}) \ \mathbf{i}-\mathbf{j}\geq 1 \\ (\Delta,\mathsf{q}_{\mathbf{j}}) \ \mathbf{i}-\mathbf{j}=0 \end{cases}$$

and the output map is

where $\{t_k, z_k\} \rightarrow \hat{u}(t)$ is defined by $\hat{u}(t) = Az_k + B$ whenever $t \in [t_k, t_k + \Delta]$ and A, B are real numbers. The <u>design parameters</u> in this feedback system are thus θ , A and B.

The problem of determining which values of x_0 and a>0 yield a Lagrange stabilized system by appropriate choice of θ , A and B has been solved by D. G. Wimpey (1977). Since the system is synchronous, the state-transition maps ϕ , δ may be replaced by one-step recursions, yielding the augmented system⁴

$$\begin{bmatrix} x(t_{i+1}) \\ q_{i+1} \end{bmatrix} = \begin{bmatrix} e^{a\Delta} & (A/a) & (1-e^{a\Delta}) \\ 0 & 0 \end{bmatrix} \begin{bmatrix} x(t_i) \\ q_i \end{bmatrix}$$

Careful consideration of these equations leads to the following cases:

Case 1: B=0

(i) If x₀<0, the system is not stabilizable.</p>

and A/a are critically stable initial conditions.

Case 2: B=0

- (i) If B>O, the results are similar to Case 1.
- (ii) If B<0, B must be chosen so that (A+B)>0, and θε[B/a, (A+B)/a] leads to a limit cycle about θ. If (A+B)<0, results similar to Case 1 are obtained Initial states x₀ε[B/a, (A+B)/a] may be stabilized.

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The purpose of this example is to illustrate how the general notation applies in a specific synchronous finite-state compensation problem, and to illustrate that indeed stabilization of continuous systems may be achieved with a very economical finite-state compensator which can be synthesized with a threshold device, flip-flop, 2-level supply and gate. The proposed representation was used to conceptualize the problem in this case, but is not in itself a design method. Note that the product space for representing the closed-loop system is immediate, given I and I.

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$${}^{4}\operatorname{sgn} [f] = \begin{cases} 1; & f \geq 0 \\ 0; & f < 0 \end{cases}$$

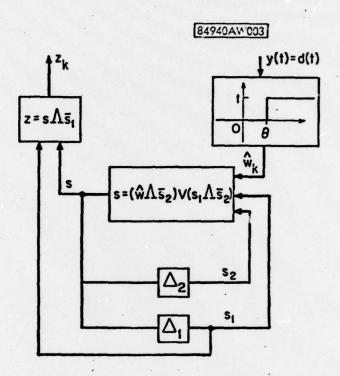


Figure 3: A Finite-State System with Feedback through delays Δ_1 , Δ_2

$$q_k^{\ell} = \begin{bmatrix} s(t_k^- \tau_k^1)^+ \\ a_k^- (t_k^- \tau_k^2)^+ \end{bmatrix} \tau_k = \begin{bmatrix} \tau_k^1 \\ \tau_k^2 \end{bmatrix}, \ell = 1, 2$$

where τ_k^1 is the elapsed time since the most recent switching of s for $t \le t_k$ ($\tau_k = 0$ if s switches at t_k), and $\tau_k^2 = t_k - t_{k-1}$ is the elapsed time since the last input transition. The key issue is to verify that δ is well-defined for one time step i.e., given $(\tau_{k-1}^l, q_{k-1}^l)$ and (t_k, θ_k) , find (τ_k^l, q_k^l) . Clearly the new input defines the last state component of t_k . If $t_{k-1} > 0$, s will switch at $t_{k-1} - \tau_{k-1}^1 + \Delta_1$ and if also $t_{k-1}^1 > \Delta_2$, s

transition will occur at $t_{k-1}^{-\tau} - t_k^{+\Delta}_2$ and $t_k^{-\tau} = 0$; or (ii) if $s(\tau_{k+1}^4) = 0$, no further changes will occur until t_k and also $t_k^{-\tau} = 0$. If $\hat{w}_{k-1} = 1$, and $t_k^{-\tau} = 1$ is large a cycle of period $t_k^{-\tau} = 1$ and duty cycle 1 will be propagated, and $t_k^{-\tau} = 1$ may be determined by $t_k^{-\tau} = 1$ mod $t_k^{-\tau} = 1$. Note that the system of Fig. 3 is a particular instance of the combined coderfinite state dynamic system portion of the general feedback system shown in Fig. 1.

DISCUSSION AND CONCLUSIONS

The results are still preliminary. The following issues can now be addressed: (1) proving when or if such a representation is

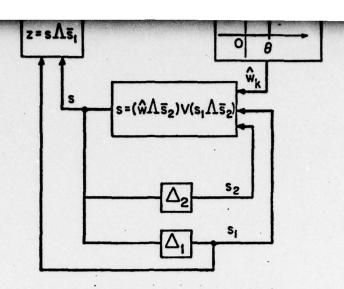


Figure 3: A Finite-State System with Feedback through delays Δ_1 , Δ_2

$$q_{k}^{2} = \begin{bmatrix} s(t_{k}^{-}t_{k}^{1})^{+} \\ a_{k}(t_{k}^{-}t_{k}^{2})^{+} \end{bmatrix} \tau_{k} = \begin{bmatrix} \tau_{k}^{1} \\ \tau_{k}^{2} \end{bmatrix}, \ ^{2} = 1,2$$

where τ_{ν}^{\perp} is the elapsed time since the most recent switching of s for $t \le t_k$ ($t_k = 0$ if s switches at t_k), and $\tau_k^2 = t_k - t_{k-1}$ is the elapsed time since the last input transition. The key issue is to verify that & is welldefined for one time step i.e., given $(\tau_{k-1}^{\ell}, q_{k-1}^{\ell})$ and (t_k, q_k) , find $(\tau_k^{\ell}, q_k^{\ell})$. Clearly the new input defines the last state component of q_k . If $\tau_{k-1}>0$, s_1 will switch at t_{k-1}^{-1} + Δ_1 and if also $\tau_{k-1}^1 > \Delta_2$, s_2 will switch at $t_{k-1}^{-1} - t_{k-1}^{1} + \Delta_2$, but by definition, these do not lead to further transitions of s in $(t_{k-1}^{1}-t_{k-1}^{1}+\Delta_{2}, t_{k-1}^{1})$, and thus s1, s2 remain constant, until tk-1. Thus for all $\tau_{k-1}^1 \ge 0$, q is known at t_{k-1}^1 (if $\tau_{k-1}^{-1} = 0$, $q_{k-1}^{-1} = q(t_{k-1}^{+})$. From t_{k-1} to t_{k} , the input has constant value w, , so it is simply a matter of simulating the transitions up to t, an interval of length t_k^{-t} and then determining if \hat{w}_k produces an s-transition at t, . Clearly this can be carried out. In fact, if $\hat{w}_{k-1} = 0$ and (τ_k^2) is large, then (i) if $s(\tau_{k-1}^+) = 1$, a single

transition will occur at $t_{k-1}^{-\tau} - t_k^{+\Delta}$ and $t_k^{-\tau} = 0$; or (ii) if $s(\tau_{k+1}^+) = 0$, no further changes will occur until t_k and also $t_k^{-\tau} = 0$. If $\hat{w}_{k-1} = 1$, and $t_k^{-\tau} = 1$ is large a cycle of period $t_k^{-\tau} = 1$, and duty cycle 1 will be propagated, and $t_k^{-\tau} = 1$ may be determined by $t_k^{-\tau} = 1$ mod $t_k^{-\tau} = 1$. Note that the system of Fig. 3 is a particular instance of the combined coderfinite state dynamic system portion of the general feedback system shown in Fig. 1.

DISCUSSION AND CONCLUSIONS

The results are still preliminary. The following issues can now be addressed: (1) proving when or if such a representation is canonical; (2) examining the properties of closed-loop dynamics obtained by state augmentation; (3) developing design and simulation methods for such systems; (4) examination of the natural operator algebra on the product space; (5) generalizations to stochastic-finite-state systems.

⁵While technically involved, the generalization of these ideas to the stochastic case should be feasible. It requires synthesis of results on continuous-time stochastic systems, stopping times, and Markov chain theory, which are already well-developed in the literature.

The primary contribution of this note is that a systematic and general method for analyzing the real-time behavior of both synchronous and asynchronous finite-state sequential machines has been discovered, and that this is representation is convenient for analyzing feedback systems. A design method based on this representation has the potential for yielding digital control algorithms which are directly implementable, thus avoiding a tedious process of approximating controllers based on ordinary calculus or, on the other hand, ion approximate representations of plant dynamics.

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